

Specification

SEMICONDUCTOR DEVICE, SEMICONDUCTOR CIRCUIT AND METHOD
OF FABRICATING SEMICONDUCTOR DEVICE

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Technical Field

The present invention relates to a semiconductor device and a semiconductor circuit, particularly to a semiconductor device and a semiconductor circuit provided with a decoupling circuit for reducing a high frequency noise that leaks through a power supply wiring.

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Background Art

In a digital circuit, high frequency noises generated incidentally to switching operations of a semiconductor element cause electromagnetic interferences. This high frequency noise mainly includes high-order harmonics of the fundamental clock frequency. For example, a part of the high frequency noises generated in an element in an LSI (Large Scale Integration) that makes a switching operation (hereinafter referred to as a switching element) propagates through the power supply wiring in the LSI and further leaks through the package of interest into the power supply wirings etc. of the printed-circuit board having the LSI mounted on.

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The high frequency noises, which propagate through the power supply wirings, couple with the package and signal wirings on the printed-circuit board, etc. in the LSI through electromagnetic induction in the propagation paths. This electromagnetic coupling causes the high frequency noises to superimpose on the signals carried through signal wirings to yield distortions of the signal voltages. Furthermore, in the case where the surge impedance

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of the power supply wiring viewed from the switching element is high, the creation of the high frequency noise brings about the creation of an electromagnetic wave, which is emitted from the signal cable and devices.

It is advantageous to arrange decoupling circuits adaptive to the
5 frequencies of the generated high frequency noises in most effective positions in order to relieve the above problems.

In the conventional decoupling circuit as described, for example, in JP H10-270643, a capacitor equivalent to a lumped constant has been arranged between a power supply wiring and a ground potential wiring, because the
10 sizes of the elements that constitute the circuit, such as a transistor, a resistor, a capacitor, etc., are small as compared with the signal wavelength corresponding to the operation frequency of the subject circuit.

Concerning other conventional decoupling circuits, JP 2001-168223 describes a technology of increasing the decoupling capacitance between
15 ground and power supply rings; and JP H06-216309 describes a technology of providing a decoupling capacitor on a lead frame of the semiconductor device. For reference, the above technologies relate to decoupling capacitors inserted between a power supply wiring and a ground potential wiring provided on the same plane and fundamentally differ in the
20 construction from the decoupling circuits of the present invention described later in that a power supply wiring and a ground potential wiring are formed in different layers.

In the circuitry in which a capacitor is employed as a decoupling circuit, it is necessary to take into account the inductance component included in
25 series with the connection terminal for the noises in a high frequency range. In other words, a capacitor includes both capacitance and inductance

components representing a capacitive characteristic at the frequency lower than the series resonance frequency of the capacitance and inductance and an inductive characteristic at the frequency higher than the series resonance frequency. Accordingly, when using a capacitor as a decoupling circuit, the
5 decoupling circuit becomes more inductive as the frequency becomes higher, resulting in degradation of the decoupling performance.

As a countermeasure to address such an issue, there is a method in which many capacitors are arranged in a distributed configuration near the package, or in the printed-circuit board in the LSI. Even if this method is
10 employed, however, the inductance of the terminals and transmission lines for connecting the capacitors and power supply wiring has an unnegligible magnitude. For this reason, it has been difficult to operate the capacitors as a decoupling circuit for a frequency range of several hundreds MHz or higher.

The operations of recent digital circuits have been sped up to have the
15 operation frequencies as high as several GHz. Consequently, it is imperative that a decoupling circuit has an impedance kept at a low value in the frequency range higher than hundreds MHz, or preferably several tens GHz, in order to suppress an electromagnetic interference and improve a signal quality. For this end, it is necessary to develop a circuit element or an
20 element structure differing from the conventional capacitor in order to be capable of retaining low impedance in a high frequency range.

It is an object of the present invention to provide a semiconductor device and a semiconductor circuit provided with a decoupling circuit capable of retaining a low impedance up to the frequency higher than several
25 hundreds MHz, and preferably several tens GHz.

Disclosure of Invention

In order to achieve the above-described object, the present invention implements a transmission line element having a ground wiring and a power supply wiring formed interposing an insulating film, on the power supply wiring on a semiconductor chip, lead or printed-circuit board, such that the capacitance per unit length of the transmission line element is increased to set the characteristic impedance of the transmission line element to an optimum value for the high frequency range. In this way, the power supply wiring inclusive of the transmission line element can have a satisfactory decoupling performance. Because this construction of the transmission line provides a decoupling circuit having an excellent decoupling performance for a higher frequency range than the conventional transmission line, the creation of the high frequency noise that propagates from a switching element to a DC power supply through a power supply wiring is suppressed to result in suppression of the electromagnetic interference and also reduction of the distortion in the waveform of a signal attributed to the high frequency noise generated by the switching element.

Brief Description of Drawings

Fig. 1 is a circuit diagram representing a structure of the best mode of the semiconductor device according to the present invention;

Fig. 2 is a circuit diagram representing an equivalent circuit of the transmission line element shown in Fig. 1;

Fig. 3 is a circuit diagram obtained by substituting a parallel admittance for the equivalent circuit of the transmission line element shown in Fig. 2;

Fig. 4 is a graph representing the relation between the characteristic impedance of the transmission line element and the value of an element S₂₁ of the scattering matrix [S];

Fig. 5 is a cross-sectional view illustrating the typical structure of the wiring formed in a semiconductor device;

Fig. 6 is a cross-sectional side view illustrating a structure of the first embodiment of the semiconductor device according to the present invention;

Fig. 7 is a flow chart representing the method of fabricating the semiconductor device of the first embodiment;

Fig. 8 is a cross-sectional side view illustrating the structure of the second embodiment of the semiconductor device according to the present invention;

Fig. 9 is a flow chart representing the first fabricating method for fabricating the semiconductor device of the second embodiment;

Fig. 10 is a flow chart illustrating the second method of fabricating the semiconductor device of the second embodiment;

Fig. 11 is a perspective view of the polysilicon and insulating film illustrating the structure of a third embodiment of the semiconductor device of the present invention;

Fig. 12 is a perspective view of the wiring illustrating the structure of a third embodiment of the semiconductor device of the present invention;

Fig. 13 is a cross-sectional view taken along an X-X' line of the semiconductor device shown in Fig. 11;

Fig. 14 is a cross-sectional view taken along a Y-Y' line of the semiconductor device shown in Fig. 11;

Fig. 15 is a flow chart illustrating the method of fabricating the

semiconductor device of the third embodiment;

Fig. 16 is a perspective view of the polysilicon and insulating film representing the structure of the semiconductor device of the fourth embodiment according to the present invention;

5 Fig. 17 is a perspective view of the wiring representing the structure of the semiconductor device of the fourth embodiment according to the present invention;

Fig. 18 is a cross-sectional view along an X-X' line of the semiconductor device shown in Fig. 16;

10 Fig. 19 is a cross-sectional view along a Y-Y' line of the semiconductor device shown in Fig. 16;

Fig. 20 is a flow chart illustrating the method of fabricating the semiconductor device of the fourth embodiment;

15 Fig. 21 is a plan view illustrating an example of the structure of a package of the semiconductor device;

Fig. 22 is an enlarged view illustrating the principal structure of the fifth embodiment of the semiconductor device according to the present invention;

20 Fig. 23 is a cross-sectional view along a Y-Y' line of the semiconductor device illustrated in Fig. 22;

Fig. 24 is a flow chart illustrating the method of fabricating the semiconductor device of the fifth embodiment;

25 Fig. 25 is an enlarged view illustrating the principal structure of the semiconductor device of the sixth embodiment according to the present invention;

Fig. 26 is a cross-sectional view along a Y-Y' line of the

semiconductor device shown in Fig. 25;

Fig. 27 is a flow chart illustrating the method of fabricating the semiconductor device of the sixth embodiment.

5 Best Mode for Carrying Out the Invention

Explanation is next presented regarding the present invention with reference to drawings.

Fig. 1 is a circuit diagram illustrating the most desirable configuration of the semiconductor device according to the present invention and Fig. 2 is
10 a circuit diagram representing an equivalent circuit of the transmission line element shown in Fig. 1.

As is shown in Fig. 1, the semiconductor device of the present invention has a structure such that a transmission line element 17 having a capacitive characteristic is inserted between a power supply wiring for
15 supplying a power supply current from a DC power supply 18 to switching element (for example, CMOS (Complementary Metal Oxide Semiconductor) inverter) 19 and the ground potential wiring. Transmission line element 17 is arranged in the nearest possible position to switching element 19 to allow a high frequency current created in switching element 19 to flow in the close
20 vicinity of switching element 19. For reference, while Fig. 1 represents the power supply wiring and the ground potential wiring directly connected through transmission line element 17, actual transmission line element 17 flows only a high frequency current between the power supply and ground potential wirings through a capacitor but flows neither a DC current nor a
25 signal current of a relatively low frequency.

As represented in Fig. 2, characteristic impedance Z_c of transmission

line element 17 is represented in terms of impedance component Z_z inserted in series between DC power supply 18 and switching element 19 and impedance component Z_y inserted in parallel with DC power supply 18. In addition, surge impedance Z_s of switching element 19 is presumed as
 5 unknown. Further, characteristic impedance Z_o of the power supply wiring depends on inductance L connected in series between DC power supply 18 and switching element 19 and the value of Z_o is estimated to be several tens to several hundreds Ω in the frequency region intended for decoupling.

Fig. 3 is a circuit diagram in which the equivalent circuit of the
 10 transmission line element shown in Fig. 2 is substituted with parallel admittance Y_c . For reference, Fig. 3 is a figure of the circuitry simplified by neglecting impedance Z_z connected in series between DC power supply 18 and switching element 19 shown in Fig. 2.

The transmission characteristic of the circuit shown in Fig. 3 is
 15 represented by scattering matrix $[S]$ shown in mathematical expression (1) below,

$$[S] = \frac{1}{Y_c' + 2} \begin{bmatrix} -Y_c' & 2 \\ 2 & -Y_c' \end{bmatrix} = \begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix} \quad (1)$$

20 where $Y_c' = Y_c/Y_o$, $Y_o = 1/Z_o$ and $Y_c = 1/Z_c$.

The reflection coefficient Γ and the transmission coefficient T of the circuit viewed from the signal input terminal in Fig. 3 (on the observer's left side of the figure = on the side of the switching element) can be represented by elements S_{11} and S_{21} of the above scattering matrix $[S]$.

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$$\Gamma = S_{11} = \frac{-Y'_c}{Y'_c + 2} = \frac{-1}{2(Z_c / Z_o) + 1} \quad (2)$$

$$T = S_{21} = \frac{2}{Y'_c + 2} = \frac{2(Z_c / Z_o)}{2(Z_c / Z_o) + 1} \quad (3)$$

where, if (impedance Z_o of the power supply wiring) \gg (impedance Z_c of transmission line element), then reflection coefficient $\Gamma = -1$, transmission coefficient $T = 0$, and thus the high frequency current generated in switching element 19 will not propagate through the power supply wiring to flow into DC power supply 18.

The present invention forms a transmission line element on the semiconductor chip, in the lead, or in the power supply wiring on the print-circuit board and thereby provides the decoupling performance to the power supply wiring including the transmission line by setting the characteristic impedance of the transmission line element to an optimum value for the high frequency range through increasing the capacitance per unit length.

The transmission line element is formed through an arrangement such that, for example, a substrate (an electric conductor of polysilicon, metal, etc.) to which the ground potential is to be applied and the wiring through which the power supply current flows are arranged on differing layers across an insulating film. For increasing the capacitance per unit length of the above transmission line element, the following approaches can be intended:

1. The insulating film provided between the wiring and the ground potential is thinned.
2. A material of a high dielectric constant is employed as an insulating film.

3. A surface area is enlarged by forming a wiring in a serpentine-curved shape, or creating corrugations on a surface of the wiring.

These three approaches can be applied in combination.

The effective transmission line length of transmission line element 17 is set to be longer than one fourth of the wavelength $((\lambda/4)/\epsilon^{1/2})$ that corresponds to the lowest frequency (hereinafter referred to as the lowest decoupling frequency) in the frequency range intended for the decoupling. As a result of this setting, the characteristic impedance of transmission line element 17 is represented as $(L/C)^{1/2}$ independent of a frequency in the frequency range intended for decoupling, wherein λ stands for the wavelength corresponding the minimum frequency, ϵ for a specific dielectric constant of the insulating film, L for an inductance per unit length of transmission line element 17 and C for a capacitance per unit length of transmission line element 17.

15 In addition, it is necessary in order to enable the decoupling performance over a wide frequency range to lengthen the effective length of transmission line element 17. It is desirable, however, to restrain an increase in a layout area of the transmission line to the minimum from the view of realization of downsizing and highly densifying a semiconductor device. For this reason, in the present invention, transmission line element 17 is formed in a serpentine-curved pattern, or to have corrugations on the surface while keeping the distance between the ground and power supply wirings constant, thereby enabling increase in the wiring width and length without increasing the layout area of the transmission line.

25 In addition, the present invention implements the transmission line element on a semiconductor chip, wherein the transmission line element is

configured to have a capacitive characteristic for the highest frequency of the high frequencies generated by the switching element on the semiconductor chip.

Further, the present invention implements the transmission line
5 element on the lead of a semiconductor device, wherein the transmission line element has a capacitive characteristic for a substantially low frequency range than the case with the transmission line element implemented on a semiconductor chip.

Alternatively, the present invention implements the transmission line
10 element on a print-circuit board, wherein the transmission line element has a capacitive characteristic for a substantially low frequency range than the case with the transmission line element implemented on a lead of a semiconductor device.

The semiconductor circuit according to the present invention is
15 mounted with a plurality of transmission line elements having different effective frequency zones arranged in a plurality of locations such as locations of a chip and a lead of a semiconductor device or a printed-circuit board in a distributed configuration in order to widen the frequency range intended for the decoupling performance and also to realize high-density
20 deployments in a semiconductor device. In this case, it is desirable to set the characteristic impedance of each transmission line element such that a voltage variation of DC power supply is 5% or less.

Furthermore, it is necessary to configure the insulating film to have a dielectric loss to some extent in order to prevent the incident wave on the
25 transmission line element from externally leaking. This dielectric loss in the insulating film is preferably as large as the heat consumption of the

electromagnetic wave incident on the transmission line element

The present invention offers a decoupling circuit having good decoupling performance up to the frequency range higher than the conventional case by adopting the transmission line element having the
5 above-described structure as a decoupling circuit. As a result, the high frequency noises, which transmit from the switching element to the DC power supply via the power supply wiring, are restrained, whereby the electromagnetic interference is reduced and also the distortion in a signal waveform caused by the high frequency noises produced in the switching
10 element is reduced.

(Embodiment)

Explanation is next presented regarding an embodiment of the present invention with reference to the drawings.

Explanation first regards the relation between the characteristic
15 impedance of the transmission line element and an element S21 of the scattering matrix [S] (transmission coefficient T).

Fig. 4 is a graph representing the relation between the characteristic impedance of the transmission line element and an element S21 of the scattering matrix [S]. For reference, Fig. 4 represents the examples in
20 which the characteristic impedances Z_0 equal 50 Ω and 100 Ω , respectively.

While the value of a characteristic impedance of a power supply wiring Z_0 generally depends on whether the wiring is formed on a printed-circuit board or it is formed on a chip of a semiconductor device, the characteristic impedance can be set to the level of approximately 50 Ω to 200 Ω . Further,
25 current digital circuits require the value of S21 to be no more than -40 dB for the decoupling performance.

As shown in Fig. 4, in the case where the characteristic impedance of the power supply wiring $Z_0 = 50 \Omega$, which is a severe condition, it is necessary to make the characteristic impedance of the transmission line element Z_c no more than 0.3Ω in order to have S_{21} no more than -40 dB .

5 Fig. 5 is a cross-sectional view typically illustrating the structure of the wiring formed in a semiconductor device.

As shown in Fig. 5, the transmission line formed in a semiconductor device is configured such that insulating film (oxide film) 21 is formed on ground substrate 20 and wiring 22 is formed on insulating film 21. Wiring 22
10 is formed using, for example, aluminum and is 1 mm in wiring length and approximately $50 \mu\text{m}$ in width. In addition, insulating film 21 is formed about 5000 \AA in film thickness using, for example, SiO_2 having a specific dielectric constant of about 4. Ground substrate 20 is formed of, for example, polysilicon doped with impurities at a high concentration and having a
15 resultant reduced resistance. Characteristic impedance Z_c of the transmission line formed of the above-described ground substrate 20, insulating film 21 and wiring 22 is about 50Ω .

Accordingly, in order to make the characteristic impedance Z_c of the transmission line element 0.3Ω or smaller, it is necessary to reduce the
20 characteristic impedance to about $1/170$ and increase the capacitance per unit length to 30,000 times for the example of the structure shown in Fig. 5.

Explanation below regards embodiments of the present invention.
(First embodiment)

Explanation is first given regarding a first embodiment of the
25 semiconductor device according to the present invention.

Fig. 6 is a cross-sectional side view illustrating a structure of the first

embodiment of the semiconductor device according to the present invention.

As represented in Fig. 6, the semiconductor device of the first embodiment has a structure in which there are provided silicon substrate 1, silicon oxide film 2 formed on silicon substrate 1, polysilicon 3 doped with high concentration impurities formed on silicon oxide film 2, insulating film 4 of a high specific dielectric constant formed of, for example, LaAlO_3 film provided on polysilicon 3 and wiring 5 formed of, for example, aluminum provided on insulating film 4.

For reference, the direction of transmission of a signal carried by wiring 5 in Fig. 6 is taken in the direction perpendicular to the surface of the page.

The transmission line element of the first embodiment has insulating film 4 formed of about 10 Å thick LaAlO_3 film having a specific dielectric constant of about 24 with polysilicon 3, insulating film 4 and wiring 5 formed in a corrugated pattern, whereby the width of the wiring is increased to about 10 times and also the capacitance per unit length is increased to about 30,000 times as compared with the general example of structure shown in Fig. 5 without changing the layout area of the transmission line. For reference, the thickness of insulating film 4 is kept constant by keeping the distance between polysilicon 3 and wiring 5 constant.

Explanation is next presented regarding the method of fabricating the semiconductor device of the first embodiment.

Fig. 7 is a flow chart representing the method of fabricating the semiconductor device of the first embodiment.

As is represented in Fig. 7, in the first embodiment, silicon oxide film 2 is first formed on silicon substrate 1 (Step S1), polysilicon 3 is formed on

silicon oxide film 2, and polysilicon 3 is processed to reduce resistance to the level of metal by implantation of impurities such as phosphorus (Step S2).

Next, patterning process is carried out on polysilicon 3 through the well-known photolithography to form corrugations (Step S3). Subsequently,
5 insulating film 4 made of LaAlO_3 film is formed in about 10 Å thickness on polysilicon 3 (Step S4) and finally wiring 5 made of aluminum is formed on insulating film 4 (Step S5).

(Second embodiment)

Fig. 8 is a cross-sectional side view illustrating the structure of the
10 second embodiment of the semiconductor device according to the present invention.

As represented in Fig. 8, the semiconductor device of the second embodiment has a structure in which there are provided silicon substrate 1, silicon oxide film 2 formed on silicon substrate 1, polysilicon 3 doped with
15 high concentration impurities, insulating film 4 of a high specific dielectric constant formed of, for example, LaAlO_3 film provided on polysilicon 3 and wiring 5 formed of, for example, aluminum provided on insulating film 4, just like the semiconductor device of the first embodiment.

The transmission line element of the second embodiment has
20 insulating film 4 formed of about 10 Å thick SrTiO_3 film having a specific dielectric constant of about 16 with the contact surfaces of the polysilicon 3 and insulating film 4 and the contact surfaces of the insulating film 4 and wiring 5 formed in a corrugated pattern, the contact surfaces being modified by finer ridges and depressions, whereby the width of the wiring is increased
25 to about 10 times and also the capacitance per unit length is increased to about 40,000 times as compared with the general example of structure

shown in Fig. 5 without changing the layout area of the transmission line.

Explanation next regards the method of fabricating the semiconductor device of the second embodiment.

Two fabrication methods are considered for fabricating the semiconductor device of the second embodiment. A first fabrication method is first explained with reference to Fig. 9.

Fig. 9 is a flow chart representing the first fabrication method for fabricating the semiconductor device of the second embodiment.

As shown in Fig. 9, in the first fabrication method, silicon oxide film 2 is first formed on silicon substrate 1 (Step S11), on which polysilicon 3 is formed, and the polysilicon 3 is processed to reduce the resistance to the level of metal by implanting phosphor ions etc (Step S12).

Next, patterning process is carried out on polysilicon 3 through the well-known photolithography technology to form corrugations(Step S13). Subsequently, further depressions are formed on the surface of polysilicon 3 through the method such as spraying wet etching solution (Step S14).

Next, insulating film 4 of SrTiO_3 is formed on polysilicon 3 (Step S15) and finally wiring 5 of aluminum is formed on insulating film 4 (Step S16).

Explanation is next presented regarding the second method of fabricating the semiconductor device of the second embodiment with reference to Fig. 10.

Fig. 10 is a flow chart illustrating the second method of fabricating the semiconductor device of the second embodiment.

As is represented in Fig. 10, in the second fabricating method, silicon oxide film 2 is first formed on silicon substrate 1 (Step S21), polysilicon 3 is formed on silicon oxide film 2, and implantation of phosphor ions etc is

implemented on the polysilicon 3 to reduce the resistance of polysilicon 3 to the level of metal (Step S22).

Next, a patterning process is carried out on polysilicon 3 through the well-known photolithography technology to create corrugations (Step S23).

- 5 Subsequently, silicon is locally grown on polysilicon 3 in a vapor-phase growth furnace while introducing silane (SiH_4) to produce protrusions (Step S24).

- Next, insulating film 4 made of SrTiO_3 film is formed on polysilicon 3 (Step S25), and finally wiring 5 of aluminum is formed on insulating film 4
10 (Step S26).

- For reference, if the lowest decouplable frequency is set to 10 GHz (wavelength $\lambda = 30$ mm) for the above-described transmission line element made up of polysilicon 3, insulating film 4 and wiring 5, then the transmission line length is $(\lambda/4)/\epsilon^{1/2}$ or greater. The length of transmission line element is
15 1.5 mm or greater in the first embodiment, because LaAlO_3 having the specific dielectric constant of about 24 is employed for insulating film 4. Further, the length of transmission line element is 1.88 mm or greater in the second embodiment, because SrTiO_3 having the specific dielectric constant of about 16 is employed for insulating film 4.

- 20 (Third embodiment)

- Fig. 11 is a perspective view of the polysilicon and insulating film illustrating a third embodiment of the semiconductor device of the present invention. Fig. 12 is a perspective view of the wiring illustrating a third embodiment of the semiconductor device of the present invention. Fig. 13 is
25 a cross-sectional view taken along an X-X' line of the semiconductor device shown in Fig. 11. Fig. 14 is a cross-sectional view taken along a Y-Y' line of

the semiconductor device shown in Fig. 11. For reference, Fig. 11 through Fig. 14 are the drawings in which silicon substrate 1 and silicon oxide film 2 are omitted from the constituent elements that make up the transmission line element.

5 As shown in Fig. 11 through Fig. 14, the transmission line element of the third embodiment has a structure in which polysilicon 3, insulating film 4 and wiring 5 are formed in a corrugated pattern in the direction (X-X') perpendicular to the signal transmission direction and also formed in a corrugated pattern in the signal transmission direction (Y-Y'). As a result of
10 this structure, the wiring width and length are increased entailing an increase in a capacitance per unit length of the transmission line element without necessitating any increase in the layout area of the transmission line element, thereby widening the range of an effective decouplable frequency of the transmission line length.

15 Explanation is next given regarding a method of fabricating the semiconductor device of the third embodiment with reference to Fig. 15.

Fig. 15 is a flow chart illustrating the method of fabricating the semiconductor device of the third embodiment.

As is represented in Fig. 15, in the third embodiment, silicon oxide film
20 2 is first formed on silicon substrate 1 (Step S31), polysilicon 3 is formed on silicon oxide film 2, and implantation of phosphor ions etc. is implemented on the polysilicon 3 to reduce the resistance of polysilicon 3 to the level of metal (Step S32).

Next, a patterning process is carried out on polysilicon 3 through the
25 well-known photolithography technology to create corrugations arranged in both of the signal transmission direction and the direction perpendicular to

the signal transmission direction (Step S33).

Next, insulating film 4 made of an LaAlO_3 film is formed about 10 \AA in thickness on polysilicon 3 (Step S 34) and finally wiring 5 of aluminum is formed on insulating film 4 (Step S34), wherein the forms of insulating film 4 and wiring 5 are corrugated in each of the signal transmission direction and the direction perpendicular to the signal transmission direction, as is the case of polysilicon 3.

It is possible in the present embodiment to increase the wiring width and wiring length to about 10 times those in the first and second embodiments without increasing the layout area of the transmission line. As a result, even if the lowest effective decouplable frequency is set to 1GHz, i.e., 1/10 that of the first and second embodiments, a length of about 1.5 mm suffices for the length of the transmission line of the transmission line element.

(Fourth embodiment)

Fig. 16 through Fig. 19 are diagrams illustrating the structure of the semiconductor device of the fourth embodiment according to the present invention. Fig. 16 is a perspective view of the polysilicon and insulating film representing the structure of the semiconductor device of the fourth embodiment according to the present invention. Fig. 17 is a perspective view of the wiring representing the structure of the semiconductor device of the fourth embodiment according to the present invention. Fig. 18 is a cross-sectional view along an X-X' line of the semiconductor device shown in Fig. 16, and Fig. 19 is a cross-sectional view along a Y-Y' line of the semiconductor device shown in Fig. 16. For reference, Fig. 16 through Fig. 19 are the drawings in which silicon substrate 1 and silicon oxide film 2 are

omitted from the constituent elements that make up the transmission line element.

As shown in Fig. 16 through Fig. 19, the transmission line element of the fourth embodiment has a structure in which polysilicon 3, insulating film 4 and wiring 5 are formed so as to have corrugations arranged in the direction (X-X') perpendicular to the signal transmission direction with each corrugation being worked to have a plurality of ridges in the side surface. As a result of this structure, the wiring width is increased entailing an increase in a capacitance per unit length of the transmission line without necessitating any increase in the layout area of the transmission line, thereby widening the range of an effective decouplable frequency of the transmission line element, just like the third embodiment.

Explanation is next given regarding the method of fabricating the semiconductor device of the fourth embodiment with reference to Fig. 20.

Fig. 20 is a flow chart illustrating the method of fabricating the semiconductor device of the fourth embodiment.

As is represented in Fig. 20, in the fourth embodiment, silicon oxide film 2 is first formed on silicon substrate 1 (Step S41), polysilicon 3 is formed on silicon oxide film 2, and implantation of phosphor ions etc. is implemented on the polysilicon 3 to reduce the resistance thereof to the level of metal (Step S42).

Next, a patterning process is carried out on polysilicon 3 through the well-known photolithography technology, corrugations arranged in the direction perpendicular to the signal transmission direction are created, and each corrugation is worked to have a plurality of ridges (Step S43).

Next, insulating film 4 made of an LaAlO_3 film is formed about 10 Å

thick on polysilicon 3 (Step S 44) and finally wiring 5 of aluminum is formed on insulating film 4 (Step S45), wherein the forms of insulating film 4 and wiring 5 are corrugated in the direction perpendicular to the signal transmission direction and their side surface have a plurality of ridges, just like polysilicon 3.

It is possible in the present embodiment as well to increase the wiring width to about 10 times that of the first and second embodiments without increasing the layout area of the transmission line. As a result, even if the lowest effective decouplable frequency is set to 1GHz, i.e., 1/10 that of the first and second embodiments, a length of about 1.5 mm suffices for the length of the transmission line of the transmission line element.

For reference, the transmission line elements illustrated in the first through fourth embodiments allow an increase in the wiring width or wiring length without increasing the layout area of the transmission line as well if it is configured so as to set the direction of transmitting a signal in the direction different by 90 degrees (i.e., in a horizontal direction with respect to the page, or in the X-X' direction). Thus, it is possible to obtain the same advantage as described above.

Further, if the transmission line element is made longer in order to attain decoupling performance for a lower frequency and consequently becomes unable to be mounted on the semiconductor chip, then it is possible to implement the transmission line element, described in connection to the above-described first through fourth embodiments, on a printed-circuit board or a lead of a package. In this regard, however, it is preferred to arrange the transmission line element near the switching element to result in less degradation in the decoupling performance.

Thus, it is preferred to implement the transmission line elements in a plurality of locations on a chip and a lead of a semiconductor device, or a printed-circuit board etc. depending on the size in order to widen the frequency zone intended for decoupling and also to realize high-density integration of a semiconductor device.

(Fifth embodiment)

The semiconductor device of the fifth embodiment is configured such that the transmission line element exemplified in each of the above-described first through fourth embodiments is implemented on a lead of a semiconductor device.

Explanation first regards a general structure of a package of a semiconductor device.

Fig. 21 is a plan view illustrating an example of the structure of a package of the semiconductor device.

As illustrated in Fig. 21, the semiconductor device has a structure having semiconductor chip 32, on which circuits are formed, fixed to die pad section 31 by means of mounting material. Internal pads (not shown) are formed on the surface of semiconductor chip 32, and the internal pads are connected respectively with a plurality of leads 33 arranged around the periphery of die pad 31 through the use of bonding wires. Die pad 31, semiconductor chip 32, bonding wires and parts of leads are sealed by resin mold layer 34.

In the present embodiment, the transmission line element described in any of the above-described first through fourth embodiments is implemented on lead for a power supply wiring (hereinafter, referred to as a power supply lead) 33-1 of a plurality of leads 33 shown in Fig. 21.

Fig. 22 is an enlarged view illustrating the principal structure of the fifth embodiment of the semiconductor device according to the present invention.

Fig. 22 is a view of power supply lead 7 and other leads of the semiconductor device in an enlarged representation showing an arrangement
5 of transmission line element 6 mounted on power supply lead 7.

Transmission line element 6 has a construction made up of polysilicon 3, insulating film (for example, LaAlO_3) 4, and wiring 5 as illustrated in any of the first through fourth embodiments.

Fig. 23 is a cross-sectional view along a Y-Y' line of the
10 semiconductor device illustrated in Fig. 22.

As shown in Fig. 23, the semiconductor device of the present embodiment has a construction in which transmission line element 6 is formed on metal ground (ground potential) surface 10 fixed to, for example, a package of a semiconductor device and epoxy resin layers 9 are formed on
15 ground surface 10 so as to sandwich transmission line element 6 of interest.

Power supply lead 7 is formed on each of epoxy resin layers 9, and transmission line element 6 and the end of power supply lead 7 on each of epoxy resin layers 9 are connected through end line 6a, 6b. Transmission line element 6 of the present embodiment is formed thinner than epoxy resin
20 layers 9. Consequently, transmission line element 6 formed thinner than insulating film 4 yields a large capacitance of transmission line element 6. For reference, Fig. 23 represents an arrangement in which lead 8 is omitted.

Explanation next regards the method of fabricating the semiconductor device of the fifth embodiment.

25 Fig. 24 is a flow chart illustrating the method of fabricating the semiconductor device of the fifth embodiment.

As represented in Fig. 24, the fifth embodiment forms first epoxy resin layers 9 having a specific dielectric constant of 4 and about 1 mm in thickness on metal ground surface 10 (Step S51).

Next, metal leads 8 (not shown) and power supply lead 7 each 1 mm wide and about 20 mm long (the length of the upper layer section only) are formed on epoxy resin layers 9 (Step S 52).

Subsequently, transmission line element 6, which is thinner than epoxy resin layers 9, is formed in the site sandwiched between epoxy resin layers 9 according to the method described in any of the above-described first through fourth embodiments (Step S53). The end portion of transmission line element 6 is bonded to power supply leads 7 formed on epoxy resin layers 9 by solder etc. For reference, the polysilicon (ground potential wiring: not shown) of transmission line element 6 is connected to metal ground surface 10.

In this construction, if, for example, the lowest decouplable frequency of transmission line element 6 is set to 1 GHz, then the length of transmission line element 6 is about 15 mm, provided that transmission line element 6 is configured in accordance with the first embodiment, and the length is about 1.5 mm, provided that transmission line element 6 is configured in accordance with the third embodiment. Further, if the lowest decouplable frequency is set to 100 MHz, then the length of transmission line element 6 is about 150 mm, provided that transmission line element 6 is configured in accordance with the first embodiment, and the length is about 15 mm, provided that transmission line element 6 is configured in accordance with the third embodiment.

If it is assumed that the length of power supply lead 7 of the

semiconductor device is 20 mm and the length of transmission line element 6 that can be mounted on the lead of interest is 15 mm, the decoupling effect can be expected in 1 GHz and higher through the use of transmission line element 6 described in the first embodiment and in 100 MHz and higher
5 through the use of transmission line element 6 described in the third embodiment.

It is to be noted that, while the above explanation has been given on the presumption that metal ground surface 10 is fixed to the package of the semiconductor device, it is possible to connect the polysilicon of the
10 transmission line element to the ground potential wiring on the print-circuit board in the case where the package lacks a ground surface.

(Sixth embodiment)

The semiconductor device of the sixth embodiment has a construction in which any of the transmission line elements exemplified in the first through
15 fourth embodiments is implemented on a lead of the semiconductor device.

Fig. 25 is an enlarged view illustrating the principal structure of the semiconductor device of the sixth embodiment according to the present invention.

Fig. 25 is an enlarged view of power supply lead 7 and other leads 8
20 of the semiconductor device illustrating an arrangement of transmission line element 6 mounted on power supply lead 7.

Fig. 26 is a cross-sectional view along a Y-Y' line of the semiconductor device shown in Fig. 25.

As represented in Fig. 26, the semiconductor device of the present
25 invention is configured such that metal ground (ground potential) surface 10 is formed on ceramic substrate (insulator substrate) 12 fixed to, for example,

a package of a semiconductor device and wiring 14 is formed on metal ground surface 10 through insulating film 13 of a high dielectric constant to yield transmission line element 41.

Ceramic layer (insulating film) 11 is formed on transmission line element 41, which is connected to power supply lead 7 formed on ceramic layer 11 of interest through a through-hole provided in ceramic layer 11.

Specifically, about 1 mm thick ceramic layer 11 made of alumina having a specific dielectric constant of 8 is formed on metal ground surface 10 and metal leads 8 (not shown) and two power supply leads 7 each 1 mm wide and about 20 mm long are formed on ceramic layer 11.

While in the first through fourth embodiments, the width of transmission line element is set to 50 μm , it is set to about 1 mm to accord with the width of power supply lead 7 in the present embodiment. High-dielectric-constant insulating film 13 is formed about 10 Å in thickness through the use of, for example, an LaAlO_3 film having a specific dielectric constant of 24.

For reference, in the present embodiment, while transmission line element 41 is not formed in a corrugated pattern, it satisfactorily clears the presumed standard, because the width of the transmission line is 20 times as compared to those of the first and second embodiments and consequently the capacitance per unit length attains about 60, 000 times that of the wiring in the general case shown in Fig. 5.

In the present embodiment, if the lowest decouplable frequency of the transmission line element is prescribed to be, for example, 1 GHz, then the length of the transmission line element becomes 15 mm or longer. Wiring 14 of transmission line element 41 is connected to power supply leads 7 in

both ends of wiring 14, and ground surface 10 is used in common for the ground-potential wiring of transmission line element 41.

Explanation next regards the method of fabricating the semiconductor device of the sixth embodiment.

5 Fig. 27 is a flow chart illustrating the method of fabricating the semiconductor device of the sixth embodiment.

As shown in Fig. 27, in the sixth embodiment, ground surface 10 formed of a metal layer is first formed on ceramic substrate 12 of alumina etc. (Step S61) and insulating film 13 about 10 Å thick formed of an LaAlO_3 film is
10 formed on ground surface 10 of interest (Step S62).

Next, wiring 14 about 1mm wide made of tungsten etc. is formed on insulating film 13 (Step S63). This piece is referred to as ceramic A.

Next, ceramic layer 11 having an opening (through-hole) formed therein is provided separately from ceramic A, and power supply leads 7
15 about 1mm wide of tungsten etc. are formed to connect the top section of ceramic layer 11, the internal wall of the through-hole, and the bottom section of the through-hole (Step S64). This piece is referred to as ceramic B.

Finally, the above-described ceramic A and ceramic B are affixed together and sintered to combine integrally (Step S65). In this step, the
20 parts of power supply leads 7 formed in the bottom portions of the through-hole provided in ceramic layer 11 are bonded to both ends of wiring 14 formed on insulating film 13.

For reference, in the above-described first to sixth embodiments, while characteristic impedance Z_c of 0.3 Ω or less is preset for the design basis of
25 the transmission line element, the characteristic impedance Z_c of an actual transmission line element depends on a required decoupling performance,

the construction, material of the leads and printed-circuit board of the semiconductor device. Thus, it is preferred to set optimum values depending on such conditions.

5 In addition, regarding the transmission line elements illustrated as examples in the above first through sixth embodiments, it is preferred to properly change the dielectric constant and thickness of the insulating film, the width and length of transmission line, the density of the corrugations, the aspect ratio of the corrugation, the shape of the corrugation, etc. according to the design basis.

10 Furthermore, regarding the foregoing first through sixth embodiments, while explanation of the methods of fabricating transmission line elements is given on the presumption of a silicon process, the methods are applicable to the fabrication process other than the silicon process such as gallium arsenide process.

15 Furthermore, the following materials can be used for the insulating film of the transmission line element: epoxy resin having the same dielectric constant of about 4 as the silicon oxide film; SiO, silicon nitride, TaO₃, TiO₂, Al₂O₃, and MgO having a specific dielectric constant of about 8; SrTiO₃ and ZrO₂ having a specific dielectric constant of about 16; LaAlO₃ having a
20 specific dielectric constant of about 24; BST (titanium oxide barium strontium) having a specific dielectric constant of about 300; and PZT (lead zirconate titanate) having a specific dielectric constant of about 1000, etc.